

Materials Science and Engineering A 427 (2006) 316-319



www.elsevier.com/locate/msea

Pyroplasticity in porcelain tiles

Adriano Michael Bernardin^{a,b,*}, Darlei Souza de Medeiros^a, Humberto Gracher Riella^b

^a Tecnologia em Cerâmica, Serviço Nacional de Aprendizagem Industrial, Rodovia BR 101 km 163, Centro, CEP 88.200-000, Tijucas, Santa Catarina, Brazil ^b Programa de Pós-Graduação em Engenharia Química, Universidade Federal de Santa Catarina,

Campus Universitário, CP 476, Trindade, CEP 88.040-900, Florianópolis, Santa Catarina, Brazil

Received 6 March 2006; received in revised form 22 April 2006; accepted 26 April 2006

Abstract

Clay bodies exhibit pyroplasticity when they are fired. Basically they get soft again in the heat of the kiln and can deform under their own weight. This property is especially important when firing products with very low porosity like porcelain tiles, due their content in melting materials. In this way, five raw materials, a kaolin, a talc, an albite, a phyllite and a clay were used in a study to form porcelain tile pastes resistant to pyroplasticity. After raw materials analysis (XRF and XRD), a mixture design with constraint limits was used to compose the pastes, resulting in 13 compositions (five factors and one centroid). All compositions were mixed, wet grounded (<44 μ m), dried and pressed (450 kgf/cm²) in rectangular plates (10 cm × 5 cm). The pyroplasticity was determined by the measure of the plate bending caused by temperature variation in an industrial roller kiln. All results were analyzed using response surfaces with data obtained by analysis of variance (ANOVA). © 2006 Elsevier B.V. All rights reserved.

Keywords: Pyroplasticity; Porcelain tile; Mixture design; Response surface

1. Introduction

Pyroplastic deformation is the bending of a ceramic specimen caused by gravity during heat treatment. It can be defined as the loss of a shape of a product during its firing. Pyroplasticity is related to an excess of liquid phases formed during firing or to a reduced viscosity of these phases. Specifically for tile ceramics fired in roller kilns, when the tiles are moving along the kiln carried by the rollers it is possible that a piece can bend to accomplish the roller rotation because it is submitted to vertical forces due its own weight. As a result the tile production is affected by curvatures arising in the final product. The pyroplastic deformation occurs more frequently in highly vitrified pastes like porcelain tiles.

The pyroplastic deformation magnitude is determined by the pyroplastic index (PI), pointing out the tendency to deformation of a specimen with fixed dimensions submitted to gravity during its firing under specific conditions. The procedure used to determine the pyroplasticity index consists in measuring the curvature of a specimen during its firing over two refractory supports [1]:

$$PI = \frac{sb^2}{l^4} \tag{1}$$

where s is the maximum deformation (cm), b is the bar thickness (cm) and l is the distance between supports (cm). The pyroplastic deformation develops in function of the vitrification of the ceramic body during its firing. As the ceramic body temperature rises inside the kiln there is a gradual increase in the amount of liquid phase formed in it. The liquid phases develop due the partial fusion of the most meltable components of the paste. As the temperature rises, the most refractory components are progressively dissolved by the liquid phases, increasing considerably the volume of the last ones.

The firing zone temperature, the heating rate and the time in which the specimens remain at the maximum temperature are variables that can affect the pyroplastic deformation because it depends on the thermal work at which the specimens are submitted [2,3].

Regarding the raw materials used to produce ceramic bodies highly vitrified, feldspars develop an important role in porcelain tile pastes. In fact, the great densification and high mechanical resistance showed by these ceramic materials after firing are due the action of feldspars [2,4,5].

^{*} Corresponding author. Tel.: +55 48 3263 8600; fax: +55 48 3263 8600.

E-mail addresses: bernardin@senai-sc.ind.br, adriano@unesc.net (A.M. Bernardin).

^{0921-5093/\$ -} see front matter © 2006 Elsevier B.V. All rights reserved. doi:10.1016/j.msea.2006.04.073

Table 1 Mixture design for the analysis of pyroplasticity in porcelain tiles

Formulation (wt.%)	Kaolin	Phyllite	Talc	Albite	Clay	
M01	50.0	20.0	10.0	10.0	10.0	
M02	20.0	50.0	10.0	10.0	10.0	
M03	20.0	20.0	40.0	10.0	10.0	
M04	40.0	20.0	10.0	20.0	10.0	
M05	20.0	40.0	10.0	20.0	10.0	
M06	20.0	20.0	30.0	20.0	10.0	
M07	40.0	20.0	10.0	10.0	20.0	
M08	20.0	40.0	10.0	10.0	20.0	
M09	20.0	20.0	30.0	10.0	20.0	
M10	30.0	20.0	10.0	20.0	20.0	
M11	20.0	30.0	10.0	20.0	20.0	
M12	20.0	20.0	20.0	20.0	20.0	
M13 (C)	26.5	26.5	17.0	15.0	15.0	

Feldspars are largely used in ceramic materials with high densification like porcelain tiles, vitreous china, porcelains and semi-grés tiles [5,6]. During firing their fusibility and ability to form eutectics with other components are remarkable, making possible to reach a high densification even at low temperatures. The main characteristic to undergo these properties is the alkali content in the mineral. The theoretical amount of potassium and sodium oxides in potassic and sodic feldspars are 16.9 and 11.8% in a weight basis, respectively [7,8]. As the alkali amount reaches the theoretical value more the commercial value of the feldspar. The amount of feldspar used in ceramic materials depends on its melting characteristic, i.e. the amount of alkali present in the mineral used [9,10].

In its turn, the use of talc in ceramic pastes results in an increase in their resistance to stains if the talc amount is higher than 1.6% in weight [3]. Also, it can raise the mechanical resistance up to 30% [7]. Some studies show the use of talc in ceramic materials seems to favor the polishing process when the porosity is low. Talc also reduces the thermal expansion coefficient of the ceramic materials and increases their whiteness when in presence of zirconium dioxide [11,12].

2. Materials and methods

Five minerals were used in this study: a clay, a kaolin, an albite, a phyllite and a talc. The chemical analysis was determined by X-ray fluorescence (Phillips PW 2400, melted sample) and the phase (mineralogical) analysis by X-ray diffraction (Phillips PW 1830, Cu K α , 0°–75°, analysis with X'Pert High-Score software).

Table 2					
Chemical	analysis	of the	raw	materials	

1-	3:		-
			•
P			B
			·
GC PG 53	C Stran	ATT A	the way is

Fig. 1. Samples on a refractory tray after sintering.

After raw material chemical and phase analysis a statistical design was used to study the influence of each mineral on the pyroplasticity of porcelain tile pastes. The chosen design was mixture design, suitable for the purpose of analysis. Regarding that not all raw materials can be used as the major component in a ceramic paste, restrictions were imposed in the design (constrained limits). Using five factors (raw materials) at two levels (maximum and minimum amount in the paste) and one general centroid 13 formulations were composed. The formulations were designated as M01–M13, the last one as the centroid (Table 1).



Fig. 2. Diffractograms of the raw materials (Q=quartz; G=goethite; K=kaolinite; M=muscovite; A=anatase; I=illite; T=talc; C=chlorite; Al=albite).

Mineral (%)	SiO ₂	Al_2O_3	TiO ₂	Fe ₂ O ₃	CaO	MgO	K ₂ O	Na ₂ O	LOI
Phyllite	73.2	15.8	0.3	1.5	0.0	0.6	2.3	0.0	5.5
Clay	62.7	22.0	2.2	1.6	0.1	0.5	0.7	0.0	9.6
Kaolin	50.0	33.8	0.4	1.3	0.0	0.4	2.0	0.0	11.7
Albite	78.0	11.6	0.1	0.2	0.7	0.4	1.1	6.3	1.0
Talc	72.1	1.5	0.1	0.8	0.1	20.1	0.1	0.0	5.8

ANOVA for the pyroplastic index	Main effects			Error			Confidence tests		
	SS	DF	MS	SS	DF	MS	F	р	R^2
Linear	6.92	4	1.73	2.81	8	0.35	4.92	0.03	0.71
Quadratic	2.75	6	0.46	0.06	2	0.03	14.56	0.07	0.99
Cubic	0	0	0	0	0	0			
Total adjusted	9.67	10	0.97						

Table 3 Variance analysis (ANOVA) for the pyroplastic index $(\times 10^{-5} \text{ cm}^{-1})$

SS, sum of squares; DF, degree of freedom; MS mean square.

The maximum and minimum limits used for kaolin were 20 and 50% (mass fraction), respectively. The limits for the other minerals were: 20–50% to phyllite; 10–40% to talc; 10–20% to albite; 10–20% to clay. The limits were established in function of the ordinary amount of each raw material in a porcelain tile paste and in function of their chemical and phase composition. In order to determine the real influence of talc on the pyroplasticity the limits used for this mineral were increased: 10–40% in weight. The literature reports the effect of talc in reducing the viscosity of the formed glass phase.

The raw materials were dried ($110 \,^{\circ}$ C, 24 h), fragmented (laboratory hammer mill), mixed according to Table 1 to form the compositions and stored. In sequence, each formulation was grounded (laboratory eccentric mill, $1.60 \,\text{g/cm}^3$, 3-4% residue in 325 mesh Tyler ($44 \,\mu$ m)), dried again ($110 \,^{\circ}$ C, 24 h), dis-

aggregated and mixed with 6% of water, forming a granulated paste. The granulate was obtained passing the mixture through an 80 mesh Tyler sieve (180 μ m), being obtained a granulate suitable for laboratory pressing. Each paste was compacted by uniaxial pressing (laboratory press, 450 kgf/cm²) in compacts with 47 mm × 100 mm and 10 mm of thickness. The compacts were dried and disposed in a refractory tray supported by their edges at 45° with the plane of the tray (Fig. 1).

The specimens of each formulation were fired in an industrial roller kiln at 1195 °C during 6 min as maximum temperature in a thermal cycle of 50 min. Four samples were chosen by chance in each running, three samples for each formulation (n = 3). After sintering the maximum deflection of the samples was measured.

The technique used to analyze the results was the multiple regression. The method validation is made by evaluation tech-



Fig. 3. Response surfaces for the pyroplastic index of the studied system.

niques used to test and estimate the adequacy and adjustment of the used model, mainly the hypothesis regression test (F and t) and the R^2 estimation.

3. Results and discussion

The chemical analysis of all raw materials are showed in Table 2. Analyzing the results apparently the most refractory minerals are the kaolin and the clay due its content in alumina, but the clay contains iron oxide (1.6 wt.%) in its composition and the kaolin contains potassium and iron oxides (1.3 and 2.0% in weight, respectively).

The phase analysis of the raw materials used in this work are shown in Fig. 2. The kaolin is formed by kaolinite and illite as major phases and quartz and goethite as contaminations. The clay is formed by kaolinite and is contaminated with quartz and anatase.

Regarding the albite, it is contaminated with quartz and muscovite, containing a small amount of potassium oxide (1.1 wt.%). Actually it is a mixed feldspar and not really an albite. The phyllite contains a small amount of potassium and iron oxides and is formed by kaolinite, quartz, goethite and muscovite and is used as a soft flux. Finally, the mineral identified as talc is contaminated with quartz and chlorite; its small amount of magnesia reveals the small amount of talc present in its composition. The ideal magnesia content in a pure talc mineral should be 32.0%(theoretical formula: $3MgO\cdot4SiO_2\cdot H_2O$).

The pyroplastic index was determined for all compositions by means of analysis of variance (ANOVA) and the results plotted in response surfaces. According to Table 3, analysis of variance for the pyroplastic index measured for all 13 formulations, the most suitable model is the quadratic model because the *F*-test is more significant for it. The quadratic model presents 93% confidence.

The results from the ANOVA analysis were plotted in response surfaces (Fig. 3). Analyzing the response surface it is clear the effect of the albite in the pyroplastic deformation. This result occurs due the content in sodium oxide in albite, besides the maximum amount of albite used was only 20% and albite is not a pure sodic feldspar. The clay also causes a strong influence in the pyroplasticity of the studied system, probably due its content in iron oxide in a non-crystalline form—none phase was identified containing iron oxide in its composition.

In its turn, the talc mineral have caused a small influence in the pyroplasticity of the system studied, besides the large amount used (40 wt.%). Apparently the presence of sodium oxide in ceramic compositions is related to the decrease in the viscosity of the formed liquid phase in the ceramic system, causing the observed pyroplasticity.

4. Conclusion

The use of mixture design in the study of ceramic formulations and the use of multiple regression and response surfaces is a powerful procedure in the evaluation of the individual effect of raw materials in the final properties of ceramic products. The strongest influence in the pyroplastic deformation was caused by the mineral albite. The clay mineral used also caused some influence, but the talc isolated had not influenced so much the pyroplastic deformation, besides the large amount of this mineral that was used.

The next step in this study will be the determination of the mineral phases formed after the sintering. Probably this new study will show the real influence of the talc content in the ceramic systems. Also, it will reveal the role played by the iron oxide in phase formation.

Acknowledgment

The authors are thankful for the XRF and XRD analyses provided by Laboratório de Análises de Minerais e Rochas (LAMIR) from Universidade Federal do Paraná (UFPR) at Curitiba, Brazil.

References

- [1] S.M. Olhero, et al., J. Am. Ceram. Soc. 84 (2001) 719.
- [2] M. Romero, et al., J. Eur. Ceram. Soc. 26 (2006) 1647-1652.
- [3] M. Dondi, et al., J. Eur. Ceram. Soc. 25 (2005) 357-365.
- [4] S.Kr. Das, et al., Appl. Clay Sci. 29 (2005) 137-143.
- [5] L. Esposito, et al., Ceram. Int. 31 (2005) 233-240.
- [6] P.M.T. Cavalcante, et al., Ceram. Int. 30 (2004) 953–963.
- [7] C. Leonelli, et al., J. Eur. Ceram. Soc. 21 (2001) 785-793.
- [8] F. Matteucci, et al., Ceram. Int. 28 (2002) 873-880.
- [9] P. Torres, et al., J. Eur. Ceram. Soc. 24 (2004) 3177-3185.
- [10] A. Tucci, et al., J. Eur. Ceram. Soc. 24 (2004) 83-92.
- [11] R. Gennaro, et al., J. Eur. Ceram. Soc. 23 (2003) 2237-2245.
- [12] M.F. Abadir, et al., Ceram. Int. 28 (2002) 303-310.